Power MOSFET 9 Amps, 20 Volts, Logic Level

N–Channel Micro–8 Leadless

EZFETs[™] are an advanced series of Power MOSFETs which contain monolithic back-to-back zener diodes. These zener diodes provide protection against ESD and unexpected transients. These miniature surface mount MOSFETs feature ultra low R_{DS(on)} and true logic level performance. EZFET devices are designed for use in low voltage, high speed switching applications where power efficiency is important. Typical applications are dc-dc converters, and power management in portable and battery powered products such as computers, printers, cellular and cordless phones.

Applications

- Zener Protected Gates Provide Electrostatic Discharge Protection
- Designed to Withstand 4000 V Human Body Model
- Ultra Low R_{DS(on)} Provides Higher Efficiency and Extends Battery Life
- Logic Level Gate Drive Can be Driven by Logic ICs
- Micro-8 Leadless Surface Mount Package Saves Board Space
- I_{DSS} Specified at Elevated Temperature

MAXIMUM RATINGS ($T_J = 25^{\circ}C$ unless otherwise noted)

Rating	Symbol	10 Secs	Steady State	Unit	
Drain-to-Source Voltage	V _{DSS}	2	V		
Gate-to-Source Voltage	V _{GS}	±12		V	
Continuous Drain Current (Note 1) $T_A = 25^{\circ}C$ $T_A = 85^{\circ}C$	Ι _D	9.0 6.4	6.0 4.3	A	
Pulsed Drain Current (tp \leq 10 µs)	I _{DM}	3	A		
Continuous Source–Diode Conduction (Note 1)	ا _s	2.9	1.4	A	
Total Power Dissipation (Note 1) $T_A = 25^{\circ}C$ $T_A = 85^{\circ}C$	P _D	3.2 1.7	1.5 0.79	W	
Operating Junction and Storage Temperature Range	T _J , T _{stg}	-55 to 150		°C	
Thermal Resistance (Note 1) Junction-to-Ambient	R_{\thetaJA}	38	82	°C/W	

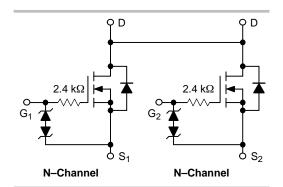
1. When surface mounted to $1'' \times 1'' FR-4$ board.

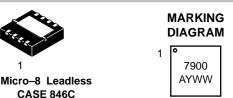


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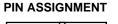
9 AMPERES 20 VOLTS $R_{DS(on)} = 26 \text{ m}\Omega$ (V_{GS} = 4.5 V, I_D = 6.5 A) $R_{DS(on)} = 31 \text{ m}\Omega$ (V_{GS} = 2.5 V, I_D = 5.8 A)

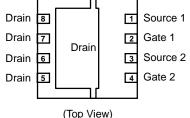




A = Assembly Location Y = Year

WW = Work Week





ORDERING INFORMATION

Device	Package	Shipping
NTLTD7900ZR2	Micro–8 LL	2500 Tape & Reel

ELECTRICAL CHARACTERISTICS (T_J = $25^{\circ}C$ unless otherwise noted)

Characteristic		Min	Тур	Мах	Unit
		-		•	
(Note 2)	V _{(BR)DSS}	20	24	_	Vdc
35°C)	I _{DSS}			1.0 20	μAdc
	I _{GSS}	-		1.0 10	μAdc mAdc
	V _{GS(th)}	0.4	0.67	1.0	Vdc
ce (Note 2)	R _{DS(on)}	-	21 27	26 31	mΩ
	C _{iss}	-	7.4	15	pF
	C _{oss}	-	237	400	
	C _{rss}	-	4.1	10	
te 3)					
	t _{d(on)}	-	0.55	1.0	μS
$(V_{GS} = 4.5 \text{ Vdc}, V_{DD} = 10 \text{ Vdc},$	t _r	-	1.17	2.0	
(Note 2)	t _{d(off)}	-	1.87	3.0	
	t _f	-	4.8	7.0	1
$(V_{00} = 4.5 Vdc lp = 6.5 Adc$	Q _T	-	12	18	nC
(V _{GS} = 4.0 Vdd, 1 <u>0</u> = 0.0 Add, V _{DS} = 10 Vdc) (Note 2)	Q ₁	-	0.7	-	
	Q ₂	I	3.7	-	
RISTICS					
$(I_{S} = 1.0 \text{ Adc}, V_{GS} = 0 \text{ Vdc})$ $I_{S} = 1.0 \text{ Adc}, V_{GS} = 0 \text{ Vdc}, T_{J} = 85^{\circ}\text{C})$ (Note 2)	V _{SD}	-	0.69 0.62	0.8 -	Vdc
	(Note 2) B5°C) (V _{DS} = 16 Vdc, V _{GS} = 0 V, f = 1.0 MHz) (V _{GS} = 4.5 Vdc, V _{DD} = 10 Vdc, I _D = 1.0 Adc, R _G = 9.1 Ω) (V _{GS} = 4.5 Vdc, I _D = 6.5 Adc, V _{DS} = 10 Vdc) (Note 2) (V _{GS} = 4.5 Vdc, I _D = 6.5 Adc, V _{DS} = 10 Vdc) (Note 2) (I _S = 1.0 Adc, V _{GS} = 0 Vdc) I _S = 1.0 Adc, V _{GS} = 0 Vdc) I _S = 1.0 Adc, V _{GS} = 0 Vdc) I _S = 1.0 Adc, V _{GS} = 0 Vdc, T _J = 85°C)	$(Note 2) \qquad V_{(BR)DSS}$ $(Note 2) \qquad V_{(BR)DSS}$ $B5^{\circ}C) \qquad I_{DSS}$ I_{GSS} I_{GSS} I_{GSS} I_{GSS} I_{GSS} I_{GSS} $(V_{DS} = 16 Vdc, V_{GS} = 0 V, C_{iss}$ C_{iss} C	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c c c c c c c c c c c c c c c c c c c $

Pulse Test: Pulse Width • 300 μs, Duty Cycle • 2%.
 Switching characteristics are independent of operating junction temperatures.

TYPICAL ELECTRICAL CHARACTERISTICS

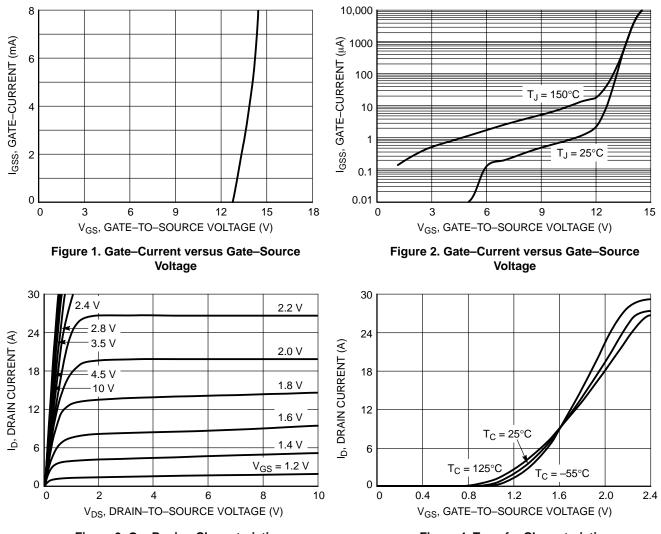




Figure 4. Transfer Characteristics

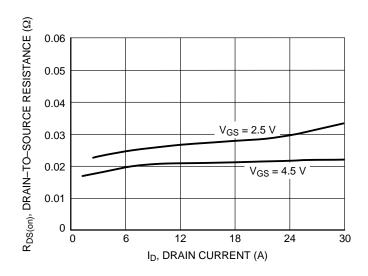


Figure 5. On–Resistance versus Drain Current

POWER MOSFET SWITCHING

Switching behavior is most easily modeled and predicted by recognizing that the power MOSFET is charge controlled. The lengths of various switching intervals (Δt) are determined by how fast the FET input capacitance can be charged by current from the generator.

The published capacitance data is difficult to use for calculating rise and fall because drain–gate capacitance varies greatly with applied voltage. Accordingly, gate charge data is used. In most cases, a satisfactory estimate of average input current ($I_{G(AV)}$) can be made from a rudimentary analysis of the drive circuit so that

 $t = Q/I_{G(AV)}$

During the rise and fall time interval when switching a resistive load, V_{GS} remains virtually constant at a level known as the plateau voltage, V_{SGP} . Therefore, rise and fall times may be approximated by the following:

$$\begin{split} t_r &= Q_2 \; x \; R_G / (V_{GG} - V_{GSP}) \\ t_f &= Q_2 \; x \; R_G / V_{GSP} \end{split}$$

where

 V_{GG} = the gate drive voltage, which varies from zero to V_{GG} R_G = the gate drive resistance

and Q_2 and V_{GSP} are read from the gate charge curve.

During the turn–on and turn–off delay times, gate current is not constant. The simplest calculation uses appropriate values from the capacitance curves in a standard equation for voltage change in an RC network. The equations are:

$$\begin{split} t_{d(on)} &= R_G \; C_{iss} \; In \; [V_{GG}/(V_{GG} - V_{GSP})] \\ t_{d(off)} &= R_G \; C_{iss} \; In \; (V_{GG}/V_{GSP}) \end{split}$$

The capacitance (C_{iss}) is read from the capacitance curve at a voltage corresponding to the off–state condition when calculating $t_{d(on)}$ and is read at a voltage corresponding to the on–state when calculating $t_{d(off)}$.

At high switching speeds, parasitic circuit elements complicate the analysis. The inductance of the MOSFET source lead, inside the package and in the circuit wiring which is common to both the drain and gate current paths, produces a voltage at the source which reduces the gate drive current. The voltage is determined by Ldi/dt, but since di/dt is a function of drain current, the mathematical solution is complex. The MOSFET output capacitance also complicates the mathematics. And finally, MOSFETs have finite internal gate resistance which effectively adds to the resistance of the driving source, but the internal resistance is difficult to measure and, consequently, is not specified.

The resistive switching time variation versus gate resistance (Figure 8) shows how typical switching performance is affected by the parasitic circuit elements. If the parasitics were not present, the slope of the curves would maintain a value of unity regardless of the switching speed. The circuit used to obtain the data is constructed to minimize common inductance in the drain and gate circuit loops and is believed readily achievable with board mounted components. Most power electronic loads are inductive; the data in the figure is taken with a resistive load, which approximates an optimally snubbed inductive load. Power MOSFETs may be safely operated into an inductive load; however, snubbing reduces switching losses.

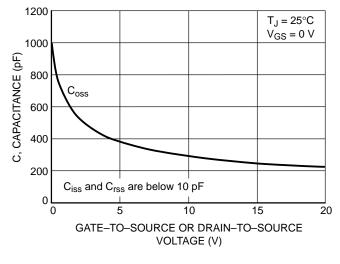
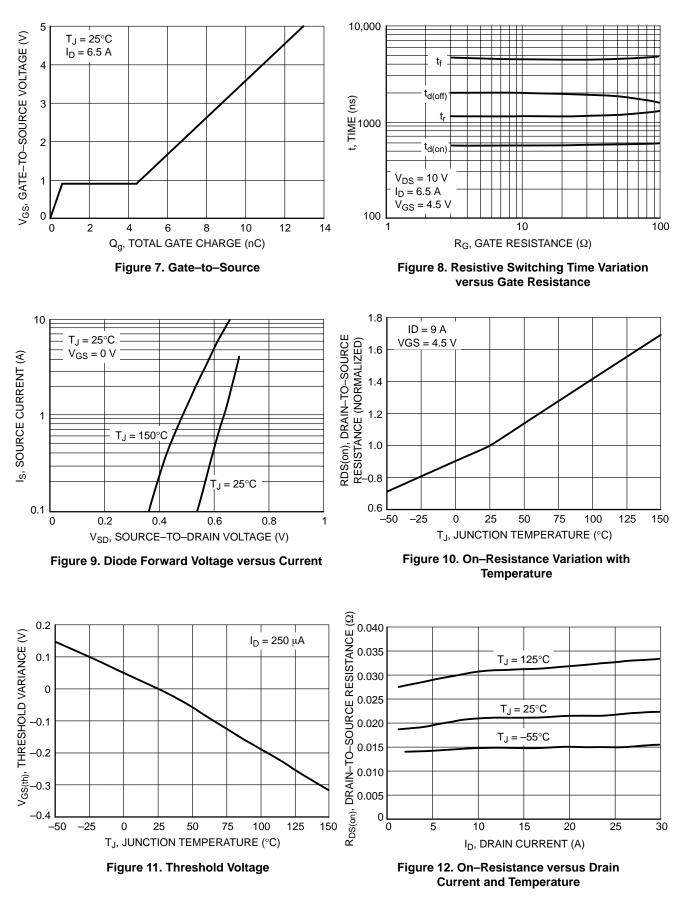
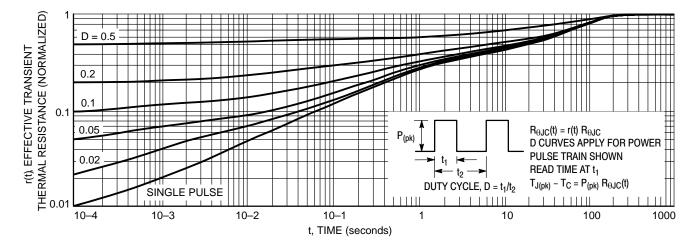


Figure 6. Capacitance Variation







TYPICAL SOLDER HEATING PROFILE

For any given circuit board, there will be a group of control settings that will give the desired heat pattern. The operator must set temperatures for several heating zones and a figure for belt speed. Taken together, these control settings make up a heating "profile" for that particular circuit board. On machines controlled by a computer, the computer remembers these profiles from one operating session to the next. Figure 14 shows a typical heating profile for use when soldering a surface mount device to a printed circuit board. This profile will vary among soldering systems, but it is a good starting point. Factors that can affect the profile include the type of soldering system in use, density and types of components on the board, type of solder used, and the type of board or substrate material being used. This profile shows temperature versus time. The line on the graph shows the actual temperature that might be experienced on the surface of a test board at or near a central solder joint. The two profiles are based on a high density and a low density board. The Vitronics SMD310 convection/infrared reflow soldering system was used to generate this profile. The type of solder used was 62/36/2 Tin Lead Silver with a melting point between 177–189°C. When this type of furnace is used for solder reflow work, the circuit boards and solder joints tend to heat first. The components on the board are then heated by conduction. The circuit board, because it has a large surface area, absorbs the thermal energy more efficiently, then distributes this energy to the components. Because of this effect, the main body of a component may be up to 30 degrees cooler than the adjacent solder joints.

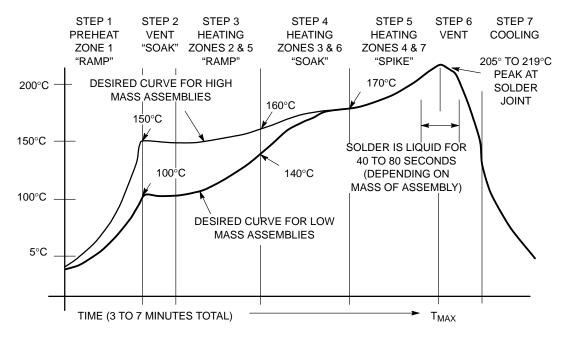
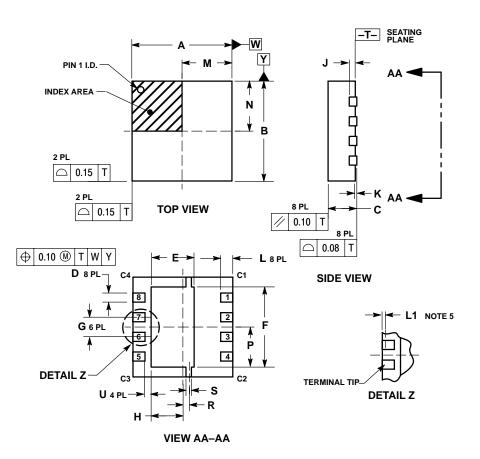


Figure 14. Typical Solder Heating Profile

PACKAGE DIMENSIONS

Micro-8 Leadless CASE 846C-01 ISSUE O



NOTES: 1. DIMENSIONS AND TOLERANCING PER ASME V14 FM 1004

- Y14.5M, 1994. 2. CONTROLLING DIMENSION: MILLIMETER. 3. THE TERMINAL #1 IDENTIFIER AND TERMINAL NUMBERING CONVENTION SHALL CONFORM TO JESD 95-1 SPP-012. DETAILS OF TERMINAL #1 IDENTIFIER ARE OPTIONAL, BUT MUST BE LOCATED WITHIN THE ZONE INDICATED. THE TERMINAL #1 IDENTIFIER MAY
- INDICATED. THE TERMINAL #1 IDENTIFIER M/ BE EITHER A MOLD OR MARKED FEATURE. 4. DIMENSION D APPLIES TO METALLIZED TERMINAL AND IS MEASURED BETWEEN 0.25 MM AND 0.30 MM FROM TERMINAL TIP. DIMENSION L1 IS THE TERMINAL PULL BACK FROM PACKAGE EDGE, UP TO 0.1 MM IS ACCEPTABLE. L1 IS OPTIONAL
- 5. DEPOPULATION IS POSSIBLE IN A SYMMETRICAL FASHION.

MILLIMETERS		
MIN	MAX	
3.20	3.40	
3.20	3.40	
0.85	0.95	
0.28	0.33	
1.30	1.50	
2.55	2.75	
0.65 BSC		
0.95	1.15	
0.25 BSC		
0.00	0.05	
0.35	0.45	
1.60	1.70	
1.60	1.70	
1.28	1.38	
0.200	0.250	
0.18	0.23	
0.20		
	MIN 3.20 3.20 0.85 0.28 1.30 2.55 0.65 0.95 0.25 0.00 0.35 1.60 1.60 1.28 0.200 0.18	

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